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Through-Silicon Via (TSV) Related Noise Coupling in Three-Dimensional (3-D)

Integrated Circuits (ICs)

A Thesis Presented

by

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Abstract of the Thesis

Through-Silicon Via (TSV) Related Noise Coupling in Three-Dimensional (3-D)

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As conventional integrated circuits are approaching the physical limits due to technology scaling, alternative and complementary technologies have become a major focus. Among various emerging technologies, three-dimensional (3-D) integration technology offers several advantages to increase performance and functionality while reducing cost. In 3-D technologies, multiple dies are stacked in a monolithic fashion where the communication among the dies is achieved by vertical through-silicon vias (TSVs). Despite important advantages, 3-D integration has certain challenges that need to be addressed. In this thesis, noise coupling due to TSVs, an important issue that degrades signal integrity, is investigated. Compact models are proposed to analyze TSV related noise coupling for different TSV types such as via-first and via-last, and different substrate grounding topologies. Figures-of-merit and design guidelines are also developed to ensure reliable 3-D circuits in the presence of TSV related noise coupling.

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List of Abbreviations

IC – Integrated Circuit

TSV – Through Silicon Via

GND - Ground

VIC – Victim

SUB - Substrate

CMOS – Complementary Metal-Oxide-Semiconductor

VLSI – Very Large Scale Integrated Circuit

Chapter 1 - Introduction

Since 1960, the integrated circuit (IC) industry aims to increase the performance and functionality of ICs while reducing power dissipation and manufacturing cost. This goal has primarily been achieved by means of technology scaling and enhancing system-level design techniques.

ITRS predicts that the physical limits of technology scaling will be reached by 2020 [1]. Numerous efforts exist to develop novel technologies alternative to conventional 2-D complementary metal-oxide semiconductor (CMOS) ICs. Carbon nanotubes, graphene based circuits, and single electron devices are examples of these efforts at the device level [2]. At the technology level, an emerging opportunity that has received considerable attention is 3-D ICs [9,10]. 3-D integration technology is highly compatible with existing CMOS manufacturing processes, thereby making 3-D technology a favorable candidate in the IC industry. Furthermore, 3-D integration is highly synergistic with conventional CMOS technology.

An important signal integrity issue in 3-D ICs is discussed in this thesis. 3-D technologies require through-silicon vias (TSVs) to transmit power, data, and clock signals among stacked dies. Since these TSVs need to pass through the substrate of the dies, noise is injected into the substrate due to the capacitive coupling between a TSV and substrate. This noise reaches the surrounding victim transistors that have a substrate bulk connection on the same plane. The amount of noise that reaches these transistors depends on several parameters. A good understanding of these parameters and the complex relationship between an aggressor TSV and the victim transistor is critical in maintaining a reliable operation with enhanced signal integrity.

This thesis consists of seven chapters. The significance of 3-D integration technology as an emerging opportunity is explained in Chapter 2. In Chapter 3, the substrate is modeled using a distributed network of resistors and capacitors (*RC* mesh). In Chapter 4, an equivalent compact model is proposed to reduce the computational complexity of the aforementioned distributed model while maintaining a reasonable accuracy. This model is verified by comparing the noise results with the results obtained from a more complicated distributed RC mesh network. The analysis results based on the proposed model are presented in Chapter 5. These results are also discussed with emphasis on the effect of different TSV types and grounding configurations on noise. Important conclusions are summarized in Chapter 6. Finally, possible future work is mentioned in Chapter 7.

Chapter 2 – Three-Dimensional (3-D) Integration Technology

In 3-D ICs multiple wafers are vertically stacked where the communication among the wafers is achieved by TSVs.

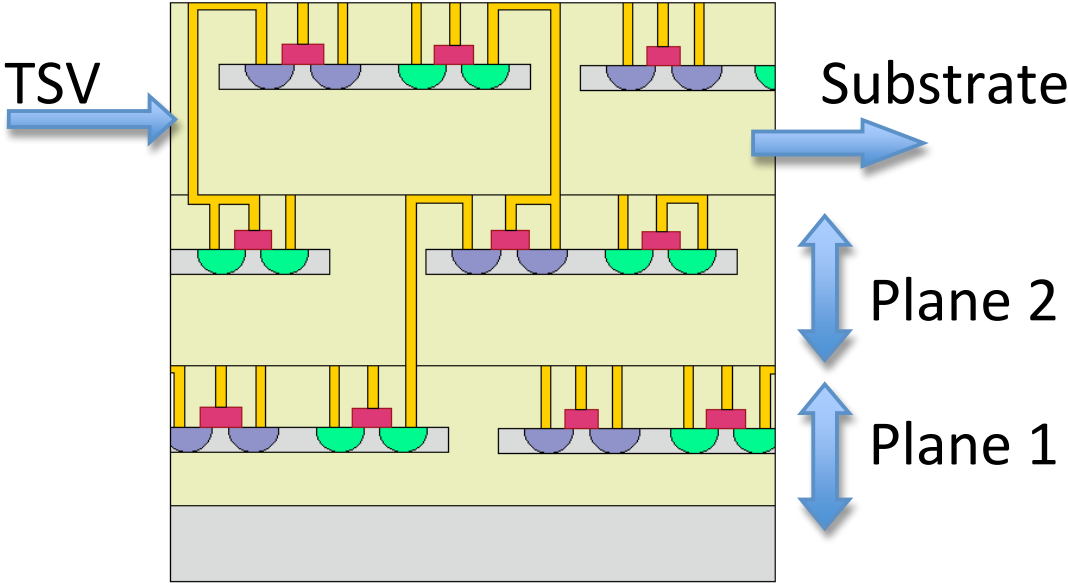


Figure 1 - TSV and substrate on a 3-D circuit.

The primary issue in 2-D ICs is increasing global interconnect lengths and related issues such as global signaling and power consumption. Continuous scaling of the transistors reduces the gate delays, but the global delay of the interconnect increases. A reduction in the length of a global interconnect is therefore required. 3-D integration provides this reduction by stacking multiple dies in a monolithic fashion. Furthermore, total active power of a 2-D circuit is considerably reduced when utilizing 3-D integration technology [3]. Another advantage of 3-D integration technology is the reduction on the physical area of the dies which is of special interest for medical, portable, and military applications. 3-D integration is therefore a prominent candidate to

continue the benefits of technology scaling. To produce a reliable 3-D circuit, multiple aspects of this new technology need to be investigated.

A critical issue in 3-D circuits is the communication between planes, as achieved by TSVs. The effect of TSVs on the design process of a 3-D circuit has been investigated in the literature[9].

There are several options to fabricate 3-D circuits. The orientation of the planes can be back-to-face, and face-to-face as illustrated respectively in Figures 2 and 3. Furthermore, there are two types of TSV fabrication techniques. Depending upon when the TSV is fabricated, the TSV technology is referred to as via-first, via-middle or via-last. The effect of these different TSVs on the circuit design process needs to be investigated. In this thesis, the effect of different TSV fabrication methods on noise coupling is addressed, as further discussed in Chapter 4.

An important challenge in 3-D circuits is the TSV induced substrate noise . This issue is a significant challenge in 3-D circuits since the TSVs pass through the substrate and inject undesirable noise signals into the substrate due to capacitive coupling between the TSV and substrate.

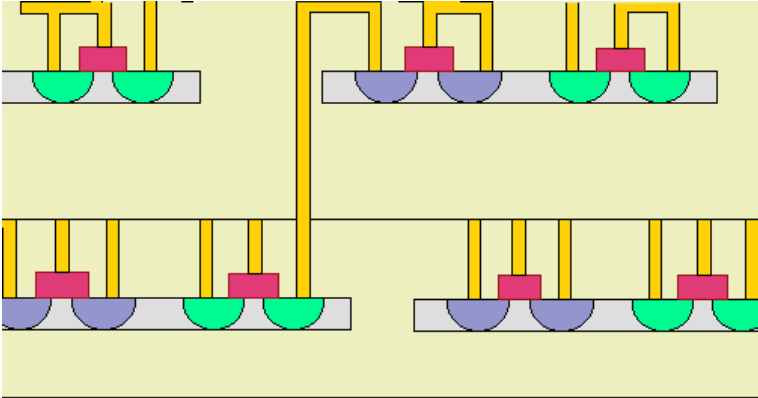


Figure 2 – Face-to-back orientation.

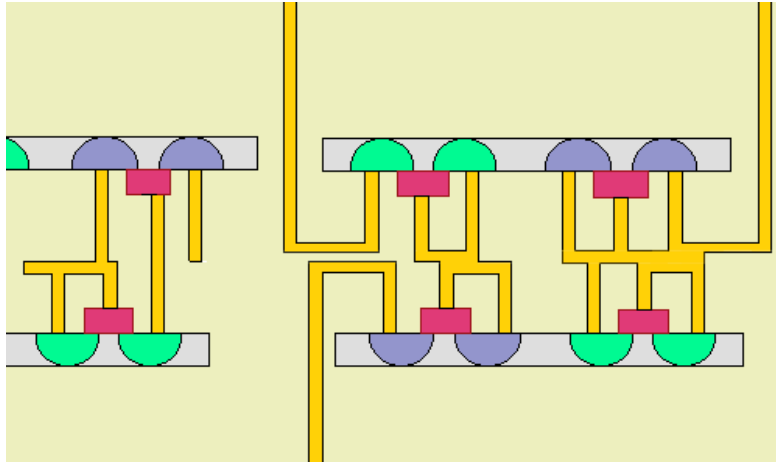


Figure 3- Face-to-face orientation.

TSV related substrate noise injection degrades the functionality and reliability of a circuit. In typical CMOS ICs, the bulks of N-type transistors are directly connected to the substrate. Any noise absorbed by these bulks therefore directly couples to the signals transmitted by these transistors. In the following chapter, an approach to model the substrate noise using an aggressor-victim methodology is described.

Chapter 3 - Models for Through-Silicon Via (TSV) and Substrate

The first step in analyzing the TSV related noise coupling is to determine an *aggressor* and *victim*. The aggressor, which is the source of noise, is in this case the TSV. The analysis is performed for two TSV fabrication techniques: via-first and via-last. As mentioned previously, these two methods differ in TSV filling material and substrate thickness, which effects the physical dimensions of the TSVs. Thus, the effect of the TSV and the corresponding noise characteristics are different.

To understand TSV related noise propagation, the TSV and substrate behavior need to be modeled. TSV and substrate models have received considerable attention in the literature [4-6]. A typical TSV and substrate model described in [4] is adopted in this work.

3.1 TSV Model

As described in [4], a TSV is represented with parasitic resistors, inductors and capacitors to the substrate as illustrated in Figure 5. The resistance and inductance represent the conductive characteristics of the TSV whereas the parasitic capacitance represents the dielectric layer between the TSV and the substrate. The TSV resistance (R_{TSV}), the TSV capacitance (C_{TSV}) and the TSV inductance (L_{TSV}) are determined by

$$R_{TSV} = \frac{1}{2} \frac{\rho_f D_{TSV}}{\pi (W_{TSV})^2},$$
$$C_{TSV} = \frac{1}{2} \frac{\pi \epsilon_{SiO_2} D_{TSV}}{\ln\left[\frac{(W_{TSV}/2) + t_{dic}}{W_{TSV}/2}\right]},$$
$$L_{TSV} = \frac{\mu_0}{4\pi} \left[2D_{TSV} \ln\left(\frac{2D_{TSV} + \sqrt{(W_{TSV}/2)^2 + (2D_{TSV})^2}}{W_{TSV}/2}\right) + (W_{TSV}/2 - \sqrt{(W_{TSV}/2)^2 + (2D_{TSV})^2}) \right].$$

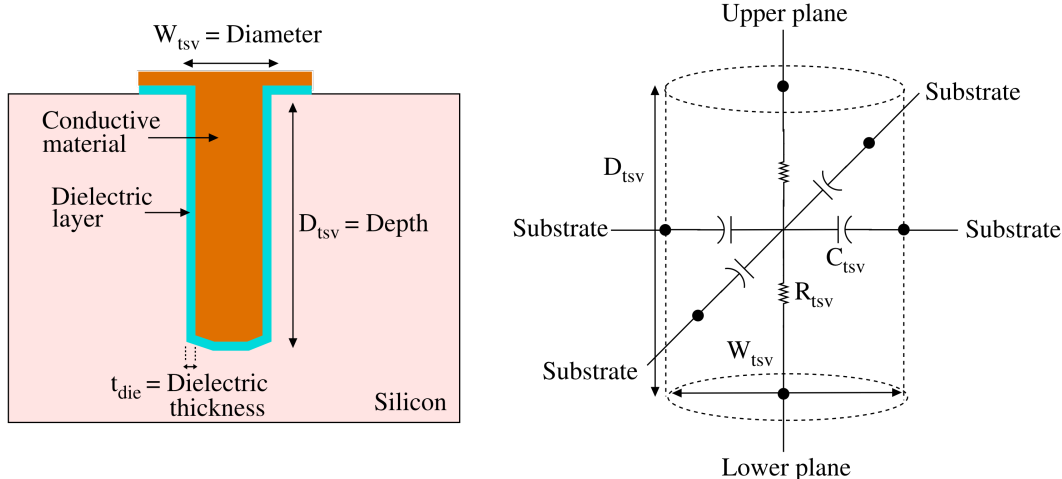


Figure 4 - TSV model [8].

where ρ_f , ϵ_0 , μ_0 , D_{TSV} , W_{TSV} and t_{die} represent, respectively, conductivity of the filling material, permittivity of the dielectric layer, vacuum permeability, TSV depth, TSV diameter, and dielectric thickness. These parameters are also illustrated in Figure 4.

3.2 Substrate Model

The substrate is modeled by a network of admittances, as depicted in Figure 6. In this model, the substrate is discretized into a large number of cuboids where each cuboid is modeled with six pairs of parallel RC s. The unit resistance R_S and the unit capacitance C_S of a cuboid are determined by

$$R_S = \frac{1}{2} \frac{\rho_s}{d_c},$$

$$C_S = \epsilon_s 2d_c,$$

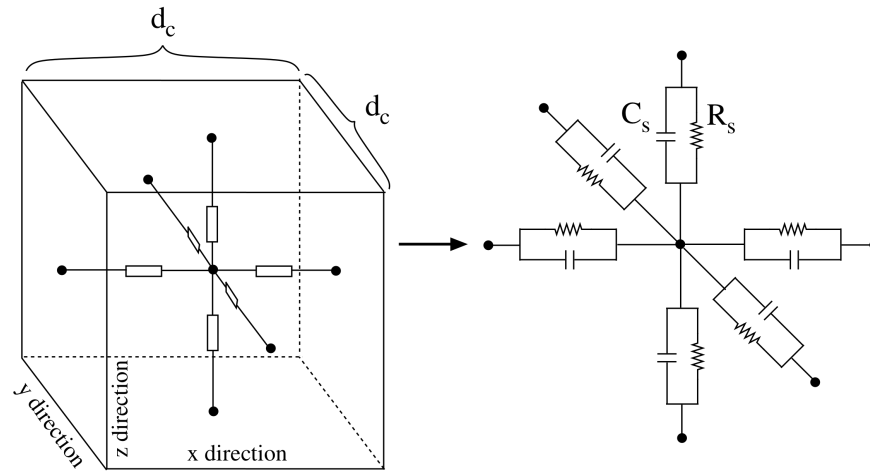


Figure 5 - Substrate model [8].

where ρ_s , ϵ_s , d_c refer, respectively, substrate resistivity, substrate dielectric permittivity and the unit length of a cuboid.

The TSV parameters illustrated in Figure 3 are dependent on the type of TSV. For example, in via-first TSVs, the filling material is polysilicon whereas in via-last TSVs copper is used as the filling material. Thus the resistivity of the filling material in both cases is significantly different.

Using these building blocks, a distributed RC mesh is obtained to model the substrate. Four cases are investigated to analyze TSV related noise coupling:

- Case 1: Via-first with custom single contact
- Case 2: Via-first with preplaced substrate contacts
- Case 3: Via-last with custom single contact.
- Case 4: Via-last with preplaced substrate contacts

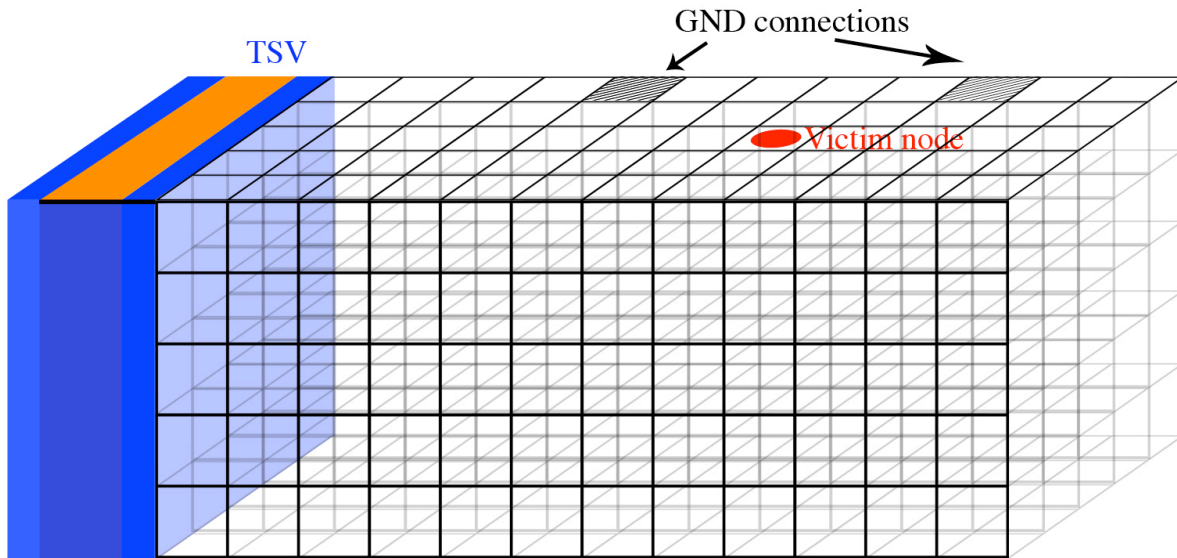


Figure 6 - Distributed RC mesh.

A portion of the substrate modeled by utilizing a distributed *RC* mesh is illustrated in Figure 6.

The top view of the same distributed *RC* mesh is illustrated in Figure 7.

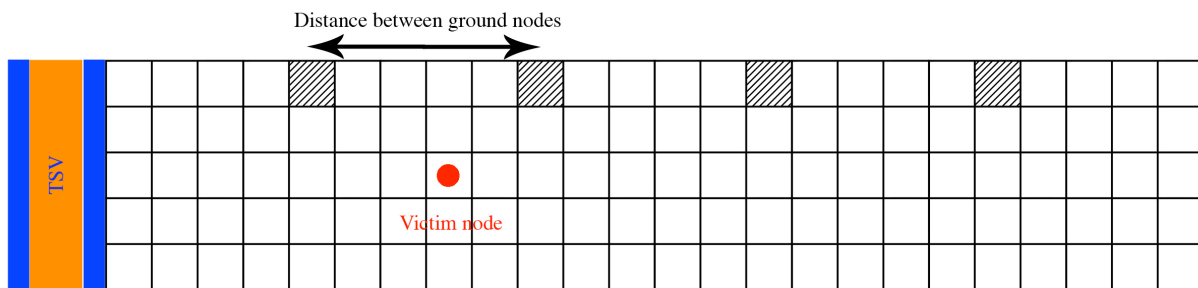


Figure 7 - Distributed RC mesh, top view.

The distributed *RC* mesh is a complicated network that captures the noise propagation through the substrate. A primary disadvantage of this model is the high computational complexity which becomes prohibitive in analyzing practical circuits with thousands of transistors. Thus, in this thesis, an equivalent compact model is developed to represent TSV related noise coupling. This

compact model is utilized to determine a safe distance between an aggressor TSV and the victim transistor beyond which the coupling noise becomes intolerable. The proposed equivalent model is described in the following chapter.

Chapter 4 – Proposed Compact Models and Verification

In the proposed model, the entire substrate network is represented by a two-port network. If the RC elements of this two-port network have negligible variation across the frequency range of interest, the reduced model can replace the more complicated substrate network described in the previous chapter. Choosing an appropriate circuit model for the two-port network is critical to obtain sufficient accuracy. Unless an appropriate model is chosen, negative impedances or undesirable variations across frequency can occur.

Two different models are investigated, as illustrated, respectively, in Figures 8 and 9. In each model, the equivalent L_{TSV} , R_{TSV} , and C_{TSV} represent the TSV parasitic impedances as described in Chapter 3. In the first model, an equivalent L -circuit model is utilized. The admittances Y_{SUB} and Y_{GND} consist of a parallel RC circuit. These admittances are obtained by performing two sets of single port AC simulations of the substrate network. This analysis is achieved by using the S-parameter simulation environment provided by Virtuoso Cadence [8]. Note that R_{VIC} in Figures 8 and 9 represents the ground configuration for the victim node such as a guard ring placed around the victim circuit. Also note that C_{Load} refers to the load capacitance of a TSV. For example, for a clock TSV this capacitance is determined by the number of registers that this TSV drives.

After analyzing the results, it is observed that the L -circuit cannot produce sufficiently accurate results. This inaccuracy is due to the inability of the L -circuit model to consider substrate contacts located in the vicinity of the victim node. The second model, however, is a sufficiently accurate representation of this phenomenon, as described below.

The primary difference between these two models is the representation of the equivalent substrate network. In the second model, referred to as the *pi*-circuit model, an additional admittance Y_{VIC} exists between the victim node and ground. Similar to the first model, the equivalent admittances are obtained by performing two port ac simulation of the substrate.

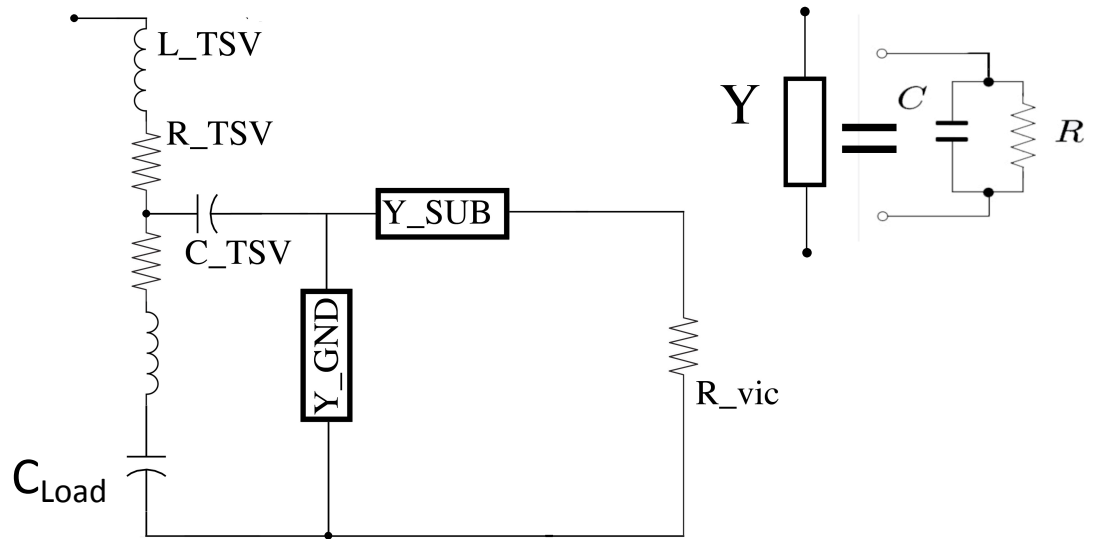


Figure 8 - Substrate *L* equivalent circuit.

As mentioned previously, the *L*-circuit model cannot consider the effect of guard rings placed close to the victim node. Such guard rings filter the noise and prevent the noise from reaching the victim, a mechanism similar to a Faraday cage. In the *L*-circuit model, however, any noise current that does not propagate toward the ground contact, propagates straight to the victim node since no other path exists for the current to flow. Furthermore, although this model represents the substrate network reasonably well, provided that the ground connection is located far from the TSV, another source of inaccuracy exists. This additional error is due to the fact that the two equivalent admittances are interdependent since the substrate network is common to both admittances. This characteristic is not considered in the *L*-circuit model. Due to these reasons, a *pi*-circuit model is developed for the equivalent two port network.

The π -circuit model consists of three admittances, Y_{GND} , Y_{SUB} and Y_{VIC} as illustrated in Figure 9. This model is more appropriate in modeling the substrate. Since, the current that flows toward the victim has an additional path to the ground, represented by Y_{VIC} . Thus Y_{VIC} can model the effect of typical noise reduction techniques such as guard rings.

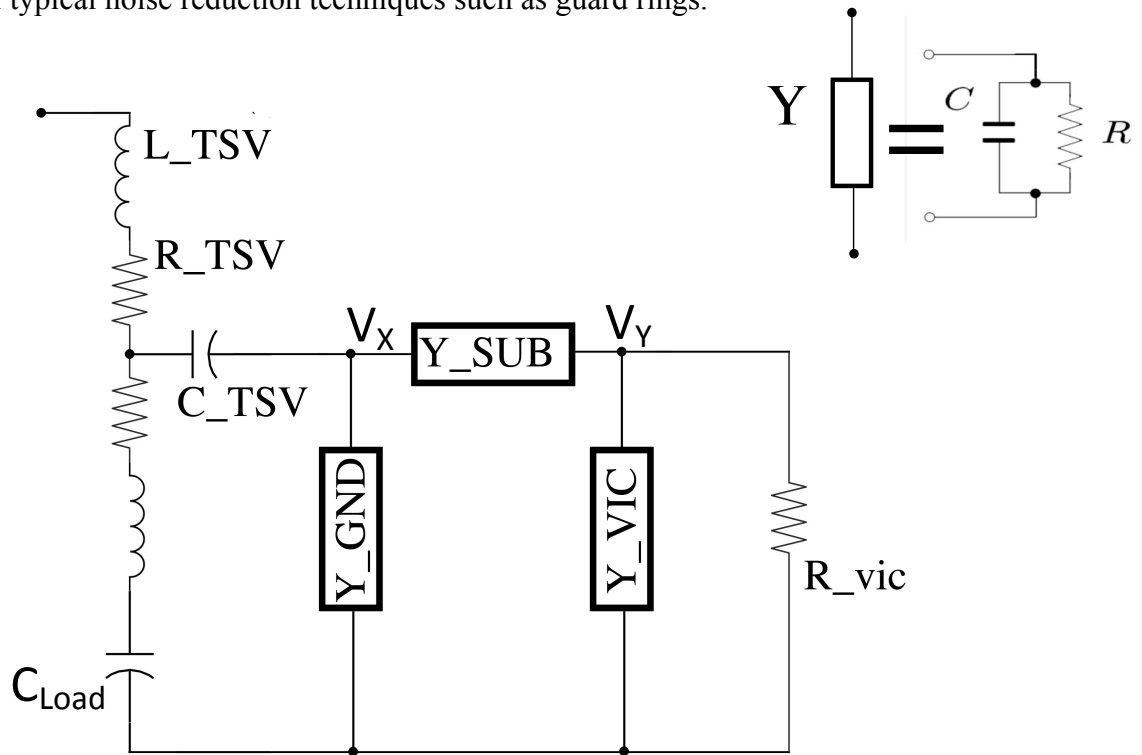


Figure 9 - Substrate π -equivalent circuit.

Theoretically, the Y -parameters of the π -circuit model can be matched to the more complicated substrate network represented as a 3-D RC mesh. This procedure includes obtaining frequency dependant elements for the π -circuit model. This dependence on frequency, however, is negligible in the frequency range of interest. The maximum change in the RC elements is less than 0.1%. Thus, a single RC value is chosen for each Y_{GND} , Y_{SUB} and Y_{VIC}

A two-port system can be characterized by utilizing Y parameters. These Y parameters, Y_{11} , Y_{12} , Y_{21} and Y_{22} are described by the following equations

$$Y_{11} = \frac{I_1}{V_1} \Big|_{V_2=0} \quad Y_{12} = \frac{I_1}{V_2} \Big|_{V_1=0}$$

$$Y_{21} = \frac{I_2}{V_1} \Big|_{V_2=0} \quad Y_{22} = \frac{I_2}{V_2} \Big|_{V_1=0}$$

Where I_1 , V_1 , I_2 and V_2 are, respectively, input current, input voltage, output current and output voltage. To obtain an accurate equivalent model, the Y parameters of the proposed pi-circuit model should be matched to the Y parameters obtained from the more complicated RC mesh network (illustrated in Figure 6). Referring to Figure 10, the Y parameters of the proposed circuit model are determined as follows

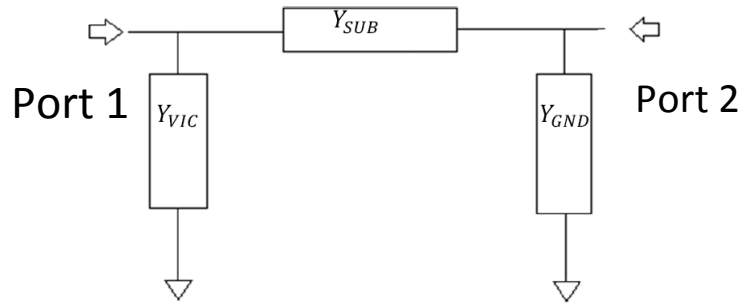


Figure 10 – π -circuit to determine Y parameters.

$$Y_{SUB} = Y_{21}$$

$$Y_{VIC} = Y_{11} - Y_{21}$$

$$Y_{GND} = Y_{22} - Y_{21}$$

These Y parameters are utilized to obtain the transfer function of the substrate represented by the π -circuit model. The following five equations describe the steps in obtaining the transconductance, $G(s)$, of the system

$$\frac{I_{out}(s)}{V_y(s)} = A = \frac{1}{Z_{SUB} + Z_{VIC}} ,$$

$$\frac{V_y(s)}{V_x(s)} = B = \frac{\frac{Z_{GND}(Z_{SUB} + Z_{VIC})}{Z_{SUB} + Z_{VIC} + Z_{GND}}}{\frac{Z_{GND}(Z_{SUB} + Z_{VIC})}{Z_{SUB} + Z_{VIC} + Z_{GND}} + \frac{1}{jC_{TSV}\omega}} ,$$

$$\frac{V_x(s)}{V_{in}(s)} = C = \frac{\frac{Z_X B_{denom}}{B_{denom} + Z_X}}{\frac{Z_X B_{denom}}{B_{denom} + Z_X} + Z_{TSV}} ,$$

where the denominator of B is

$$B_{denom} = \frac{Z_{GND}(Z_{SUB} + Z_{VIC})}{Z_{SUB} + Z_{VIC} + Z_{GND} + \frac{1}{jC_{TSV}\omega}} ,$$

$$G(s) = A \times B \times C .$$

To evaluate the accuracy of the proposed equivalent π -circuit model, the transconductance described is compared with the transconductance obtained from the distributed RC mesh network. The results of this comparison are illustrated in Figure 11.

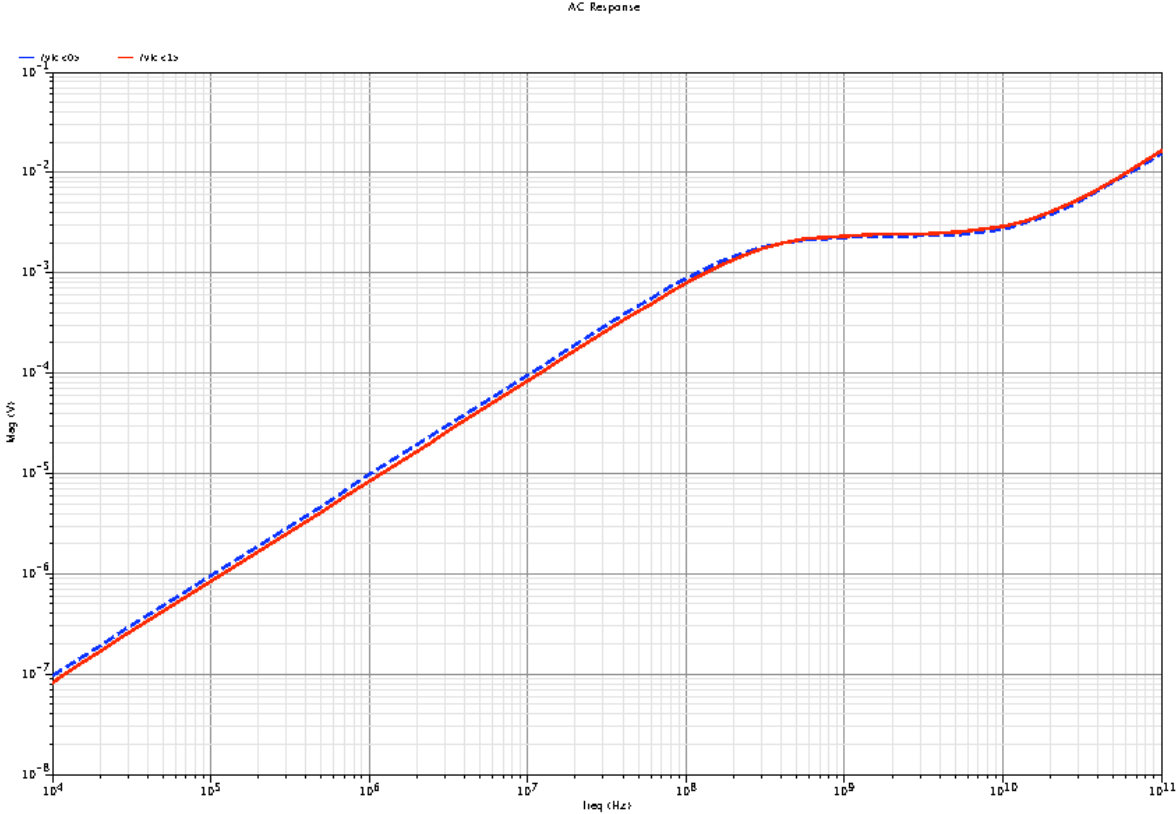


Figure 11 - Distributed RC mesh transfer function (dashed). Equivalent π model transfer function (solid).

As depicted in this figure, the transconductance obtained from these two networks are sufficiently close.

After obtaining an equivalent π -circuit model to represent the complicated substrate network, in the next step, a relationship between the Y parameters of the equivalent network and the physical distance between the TSV victim and ground nodes is investigated. This relationship is highly critical to obtain as a that determines the physical area where transistors should be placed. An

accurate characterization of the safe distance is significant for certain applications such as 3-D core memory stacks and heterogeneous 3-D ICs where highly sensitive analog/RF blocks coexist with aggressor TSVs.

To find a relationship between Y_{SUB} , Y_{GND} , Y_{VIC} , and the physical distances, a series of simulations are performed for different cases. The large amount of data obtained by these simulations are represented by specific functions with two variables. These different cases are described in the following:

Case 1: Via-first TSV with a single custom ground node

In this case, d_1 (μm) and d_2 (μm) refer respectively to the distance between the TSV and the victim node, and the distance between the TSV and ground.

The appropriate fitting function used to model the dependence of RC elements on distance is

$$F(d_1, d_2) = A + E.d_1 + B.\ln(d_1) + C.d_2 + D.\ln(d_2)$$

where A , B , C , D , and E are fitting coefficients. This fitting function is obtained after thorough simulations of the distributed RC mesh network. These results represent the dependence of Y elements on distance and are illustrated in Figures [12-18]. For example, the dependence of Y_{GND} , R_{GND} , and C_{GND} on the two distances is illustrated in Figures 12 and 15. Similarly, the remaining elements of the Y parameters are illustrated in Figures [12-17].

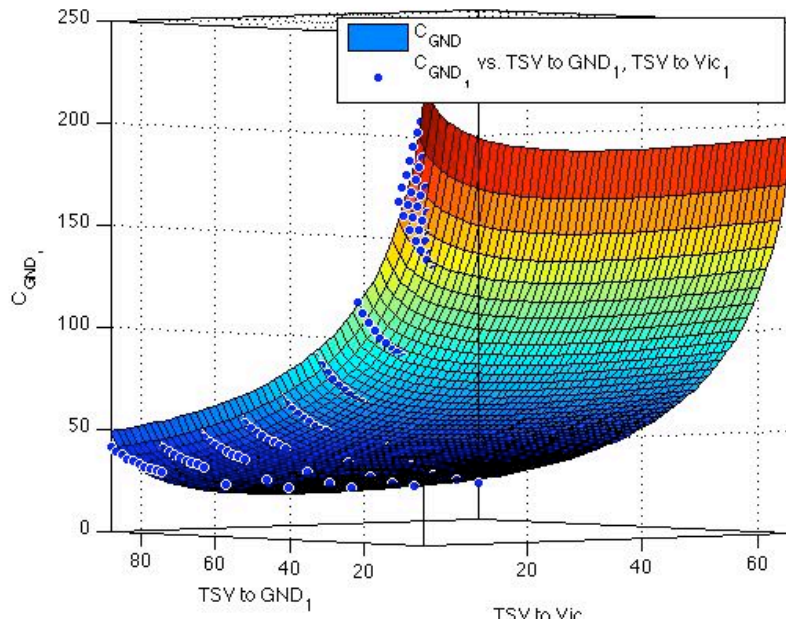


Figure 12 - Case 1, C_{GND} vs. d_1 and d_2 .

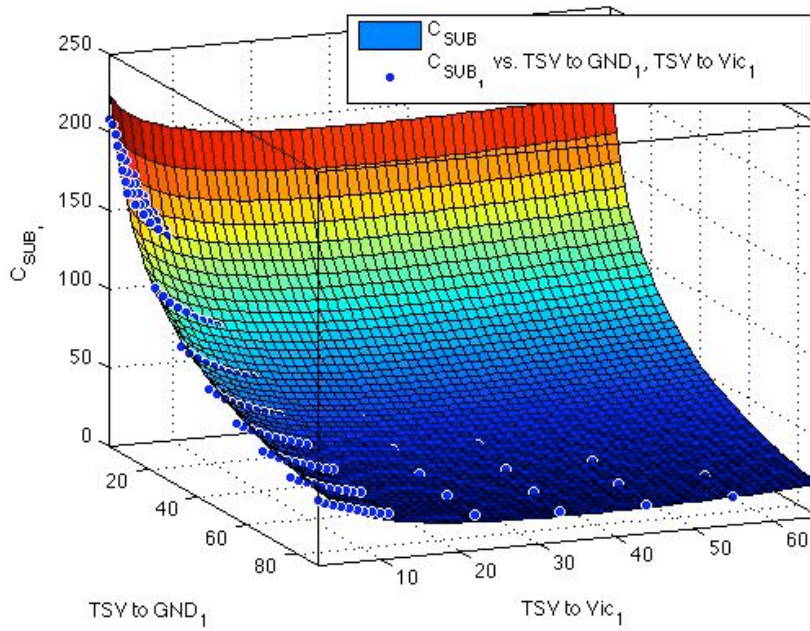


Figure 13 - Case 1, C_{SUB} vs. d_1 and d_2 .

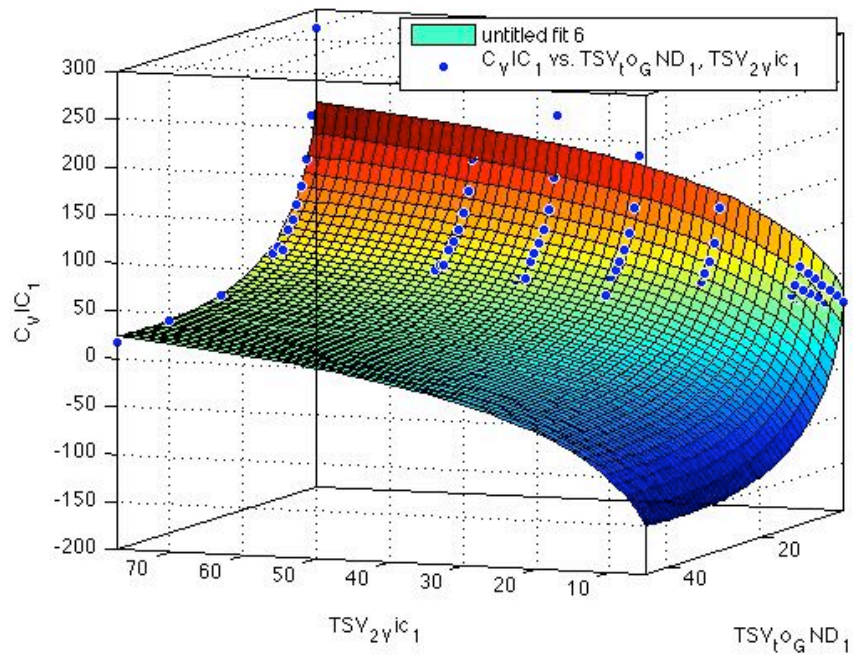


Figure 14 - Case 1, C_{VIC} vs. d_1 and d_2 .

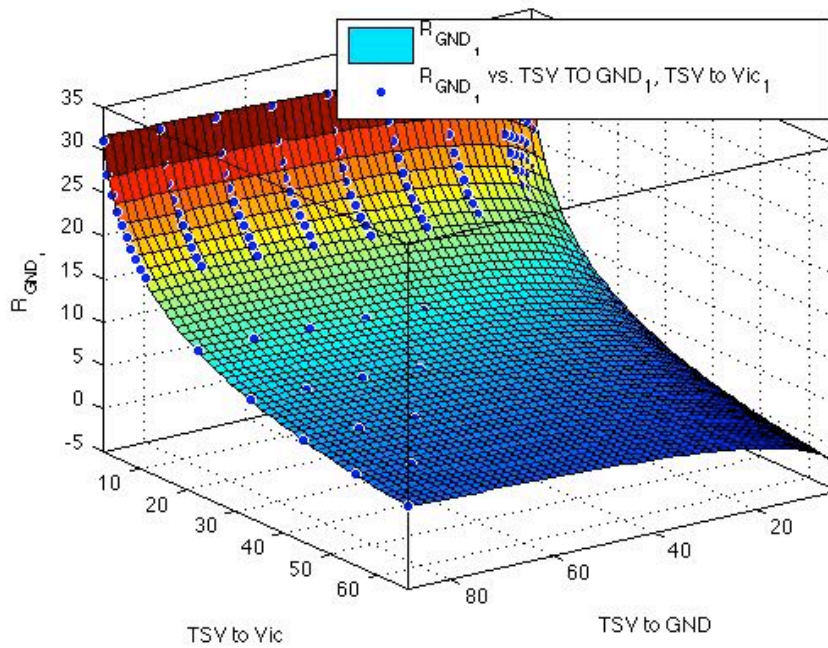


Figure 15 - Case 1, $1000/R_{GND}$ vs. d_1 and d_2 .

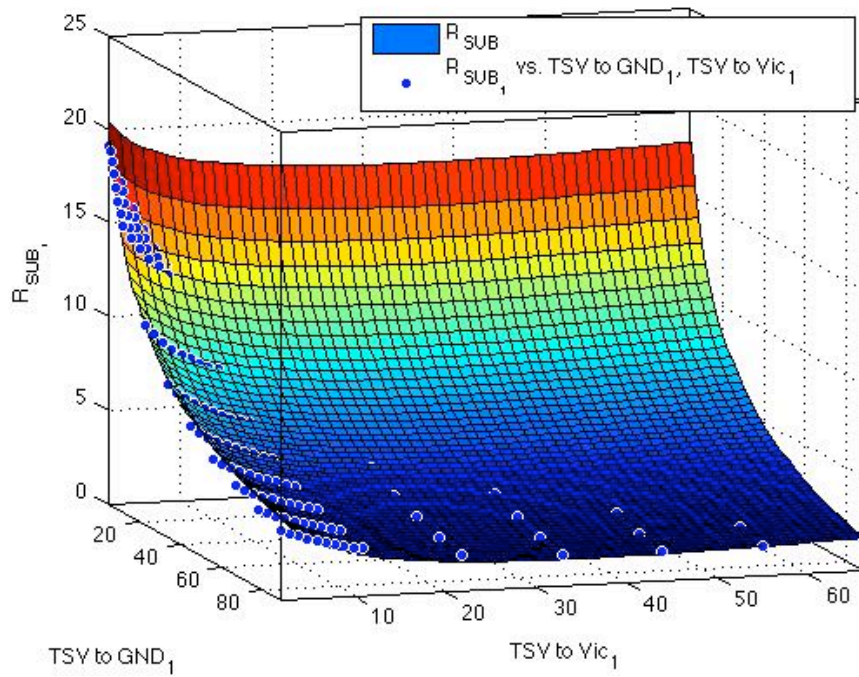


Figure 16-Case 1, $1000/R_{SUB}$ vs. d1 and d2.

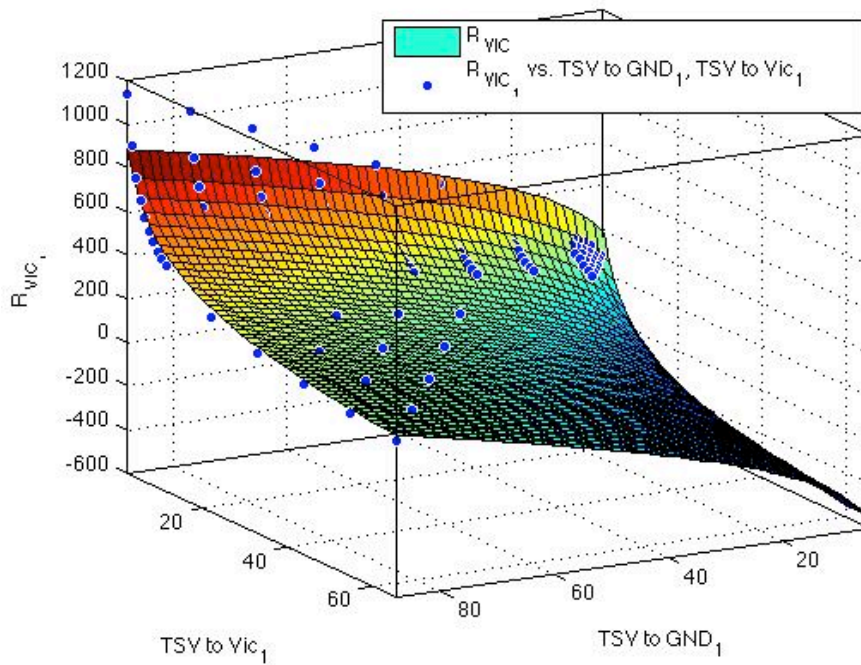


Figure 17 - Case 1, R_{VIC} vs. d1 and d2.

Note that the dots in these graphs are obtained from the 3-D RC mesh network. Alternatively, the surface represents the fitting functions. For Case 1, the coefficients A , B , C , D , and E are listed in Table 1.

Table 1 - Fitting coefficients Case 1.

	$1000/R_{GND}$ ($K\Omega$)	C_{GND} (af)	R_{SUB} ($K\Omega$)	C_{SUB} (af)	R_{VIC} ($K\Omega$)	C_{VIC} (af)
	$1000/F(d1,d2)$	$F(d1,d2)$	$1000/F(d1,d2)$	$F(d1,d2)$	$F(d1,d2)$	$1000/F(d1,d2)$
A	28.31	301.3	27.09	326.7	151.6	13.53
B	0	-0.2752	0	0.4083	3.7	0.3322
C	0	0.6591	0	0.4834	1.788	0.1675
D	-8.142	-96.94	-0.9812	-17.26	-244.6	-22.53
E	1.982	30.09	-5.109	-67.55	128.3	12.01

Note that every column in this table corresponds to one of the graphs illustrated Figures [12-17]. Also note that the maximum error of this fitting function is less than 10%.

Case 2: Via-last TSV with a single custom ground node

A similar analysis is performed but the TSV is replaced with a via-last TSV. The results of this analysis are illustrated in Figures [18 – 23]. The corresponding fitting coefficients are provided in Table 2.

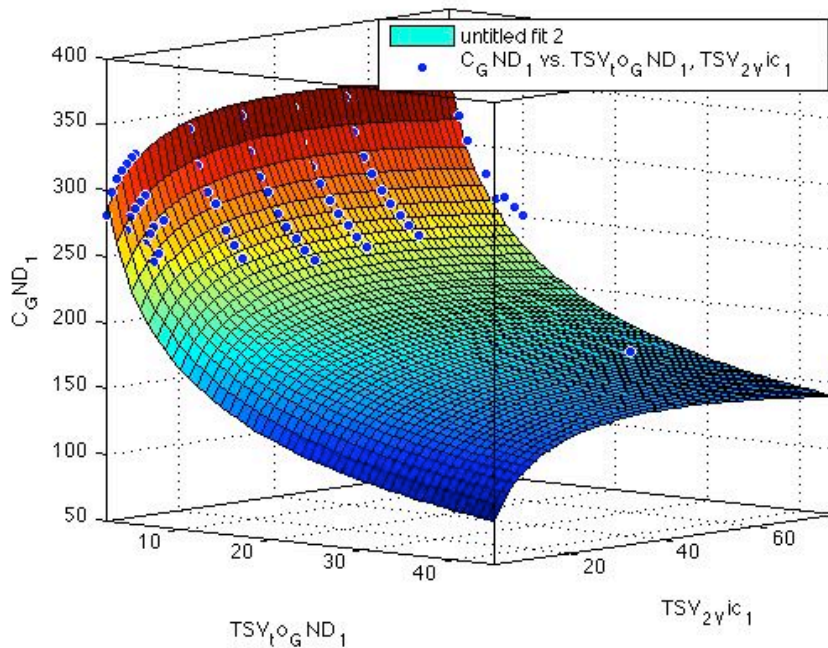


Figure 18 - Case 2, C_{GND} vs. $d1$ and $d2$.

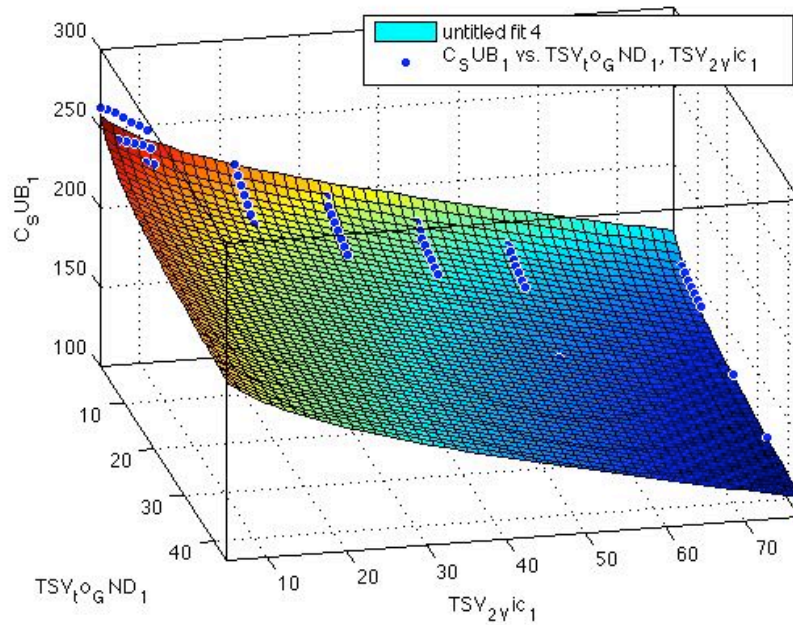


Figure 19 - Case 2, C_{SUB} vs. d_1 and d_2 .

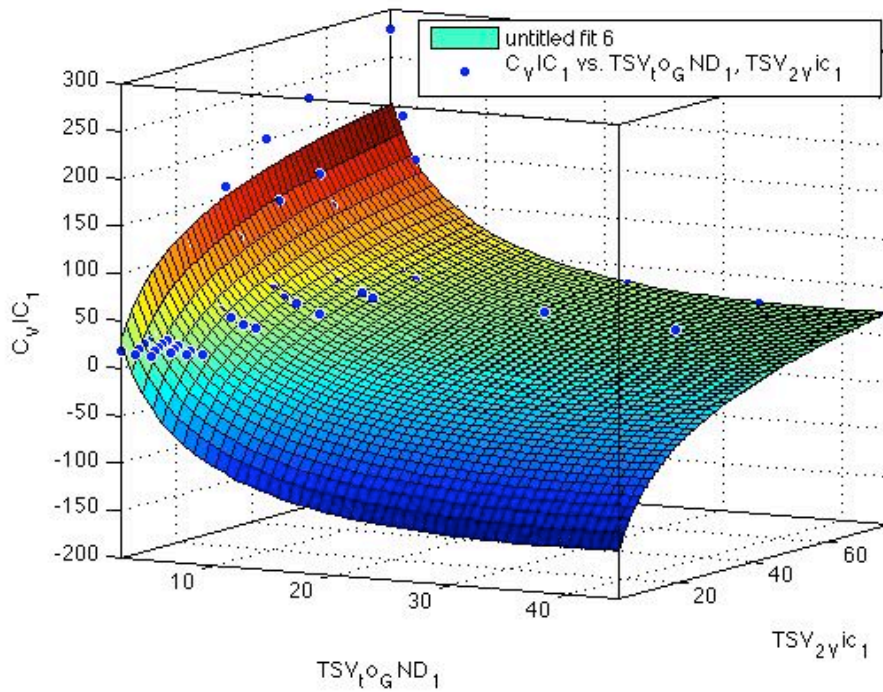


Figure 20 - Case 2, C_{VIC} vs. d_1 and d_2 .

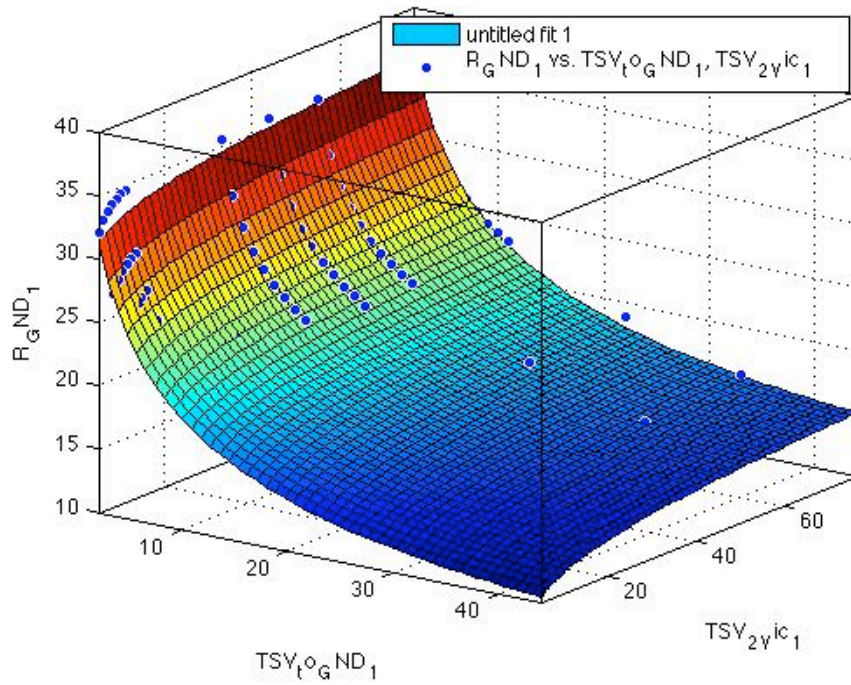


Figure 21 - Case 2, $1000/R_{GND}$ vs. d_1 and d_2 .

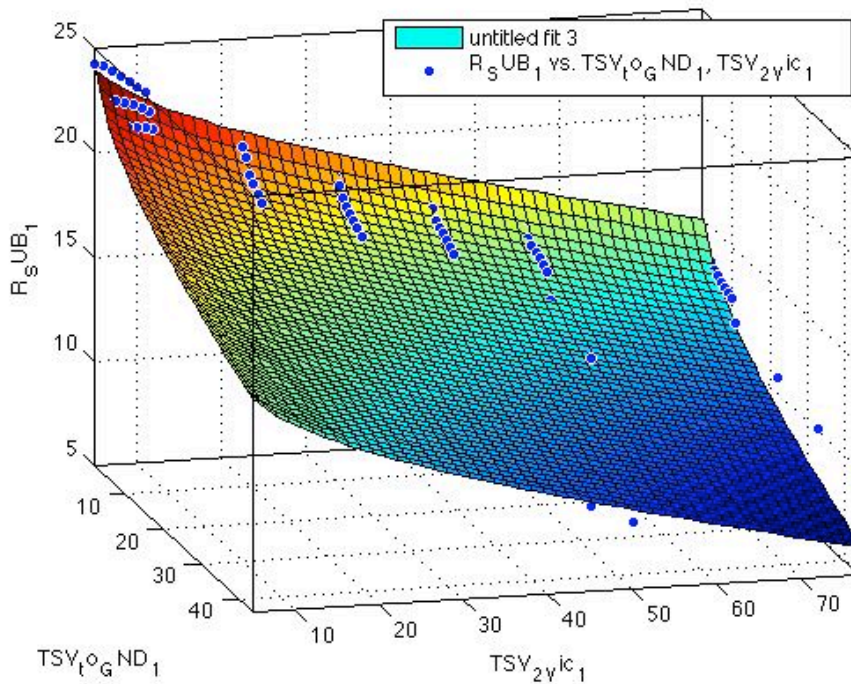


Figure 22-Case 2, $1000/R_{SUB}$ vs. d_1 and d_2 .

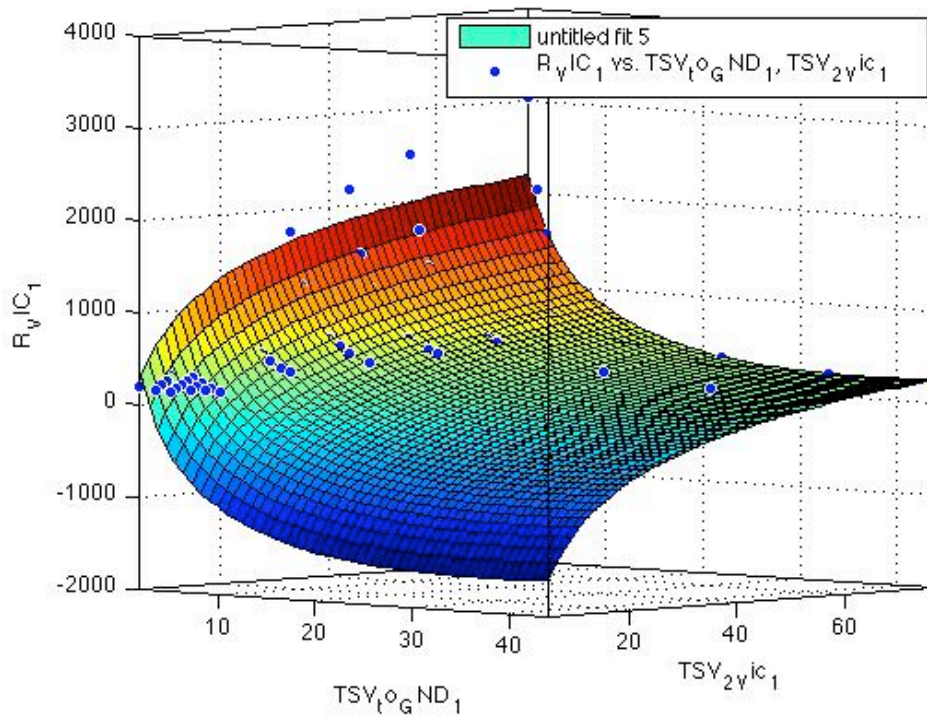


Figure 23 - Case 2, R_{VIC} vs. $d1$ and $d2$.

Table 2 - Fitting coefficients Case 2.

	$1000/R_{GND}$ (K Ω)	C_{GND} (af)	R_{SUB} (K Ω)	C_{SUB} (af)	R_{VIC} (K Ω)	C_{VIC} (af)
	$1000/F(d1,d2)$	$F(d1,d2)$	$1000/F(d1,d2)$	$F(d1,d2)$	$F(d1,d2)$	$1000/F(d1,d2)$
A	34.37	263.7	27.97	298.5	9.117	101.4
B	0.135	0.7956	-0.07299	0	0	0.1799
C	0	-1.129	-0.06895	-0.7594	0.04936	0.5132
D	1.7	50.72	-1.436	-16.34	-3.465	-37.48
E	-8.623	-77.3	-1.816	-14.91	1.82	17.89

Case 3: :Via-first with preplaced substrate contacts

A similar analysis is performed with a via-first TSV, but the single ground connection is replaced with preplaced substrate contacts. The results of this analysis are illustrated in Figures [24 – 29]. The corresponding fitting coefficients are provided in Table 3.

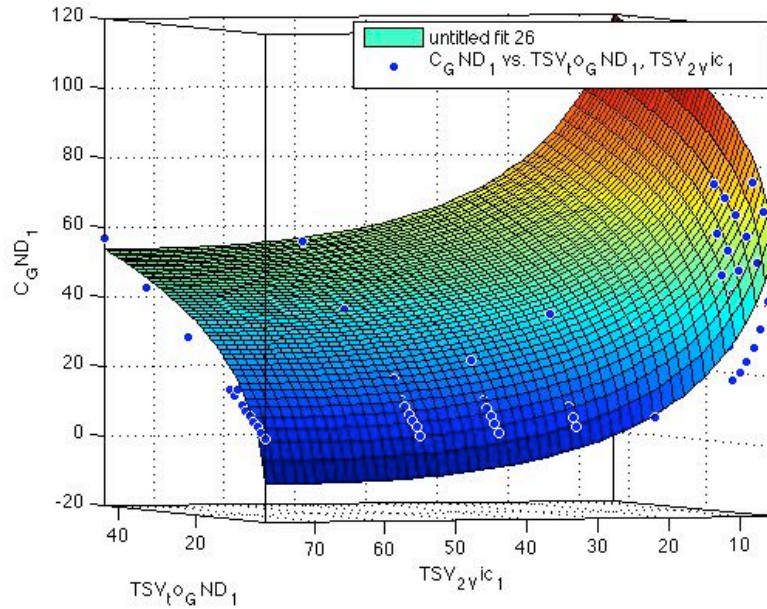


Figure 24-Case 3, C_{GND} vs. $d1$ and $d2$.

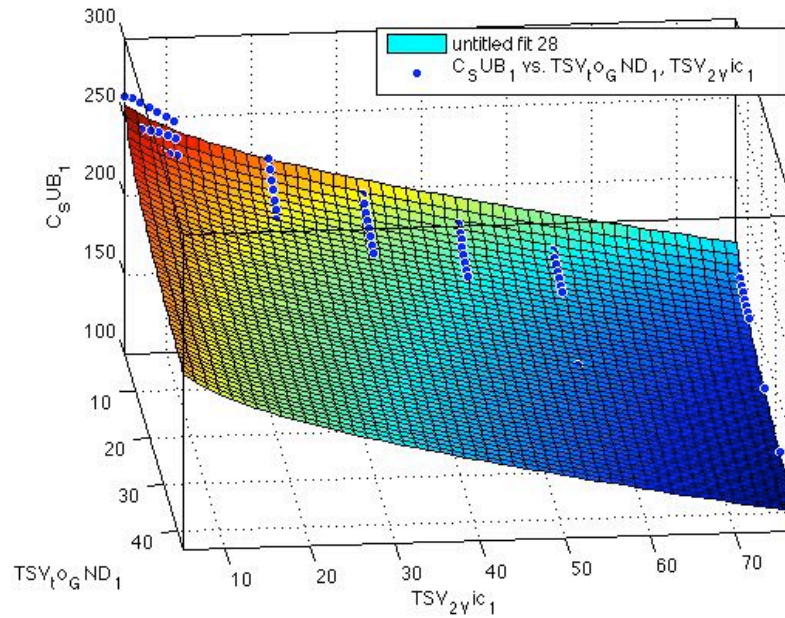


Figure 25-Case 3, C_{SUB} vs. $d1$ and $d2$.

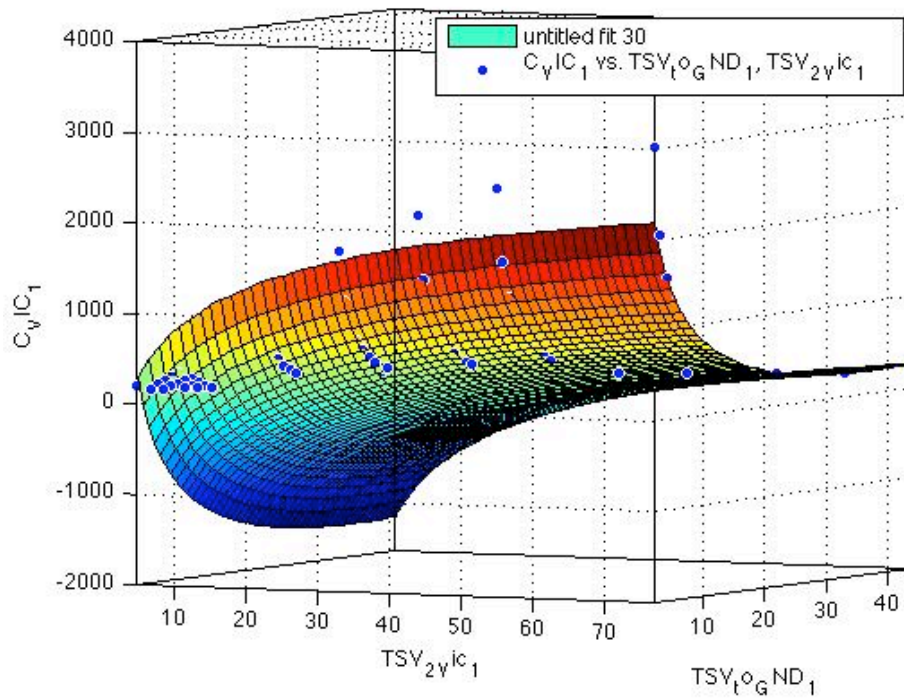


Figure 26-Case 3, C_{VIC} vs. $d1$ and $d2$.

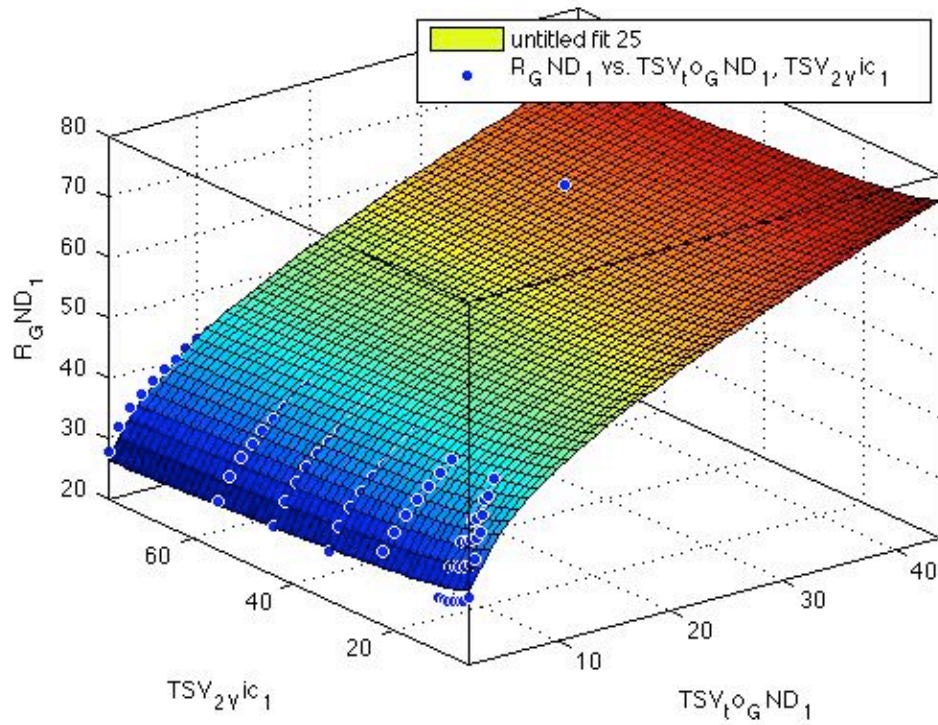


Figure 27-Case 3, R_{GND} vs. $d1$ and $d2$.

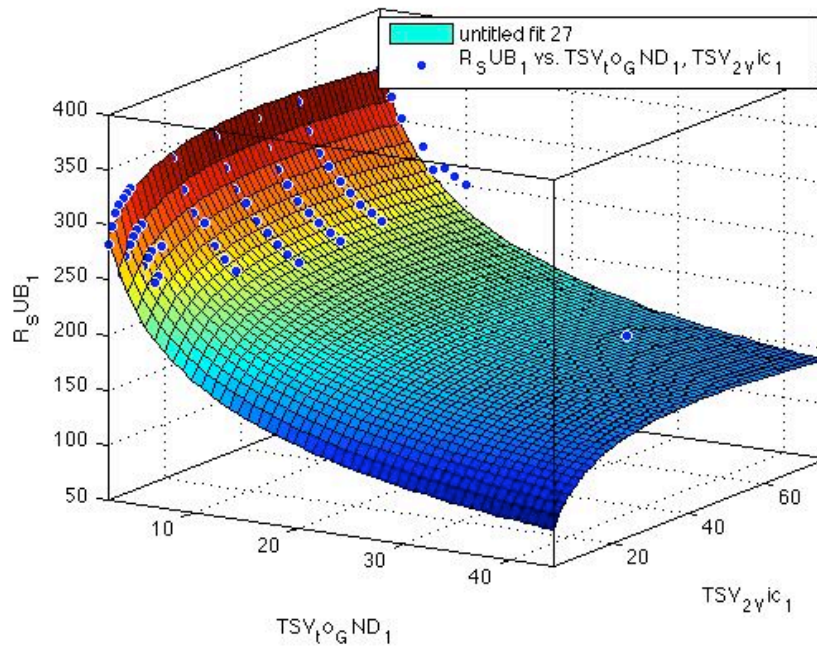


Figure 28-Case 3, R_{SUB} vs. $d1$ and $d2$.

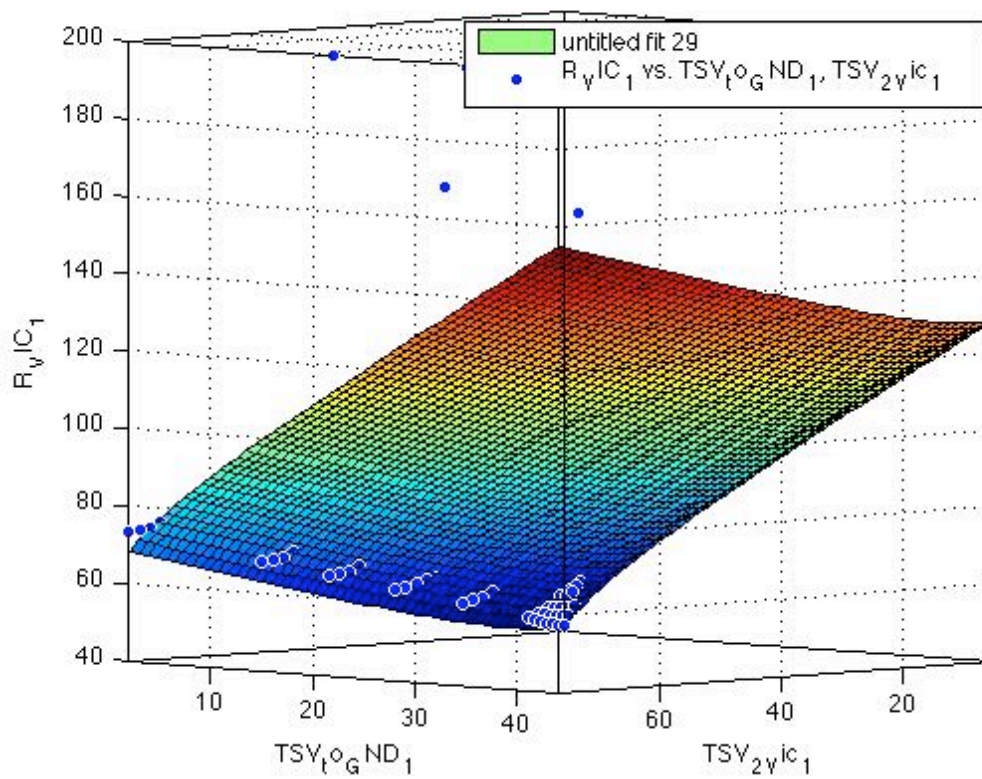


Figure 29-Case 3, R_{VIC} vs. $d1$ and $d2$.

Table 3 - Fitting coefficients Case 3.

	$1000/R_{GND}$ (K Ω)	C_{GND} (af)	R_{SUB} (K Ω)	C_{SUB} (af)	R_{VIC} (K Ω)	C_{VIC} (af)
	$1000/F(d1,d2)$	$F(d1,d2)$	$1000/F(d1,d2)$	$F(d1,d2)$	$F(d1,d2)$	$1000/F(d1,d2)$
A	28.87	101.4	263.7	298.5	9.117	101.4
B	0.446	0.1799	0.5789	0	0	0.132
C	0.0182	0.5132	-1.129	-0.7594	0.04936	0.37.87
D	-1.737	-37.48	50.72	-16.34	-3.465	-28.4
E	8	17.9	-77.3	-14.91	1.82	18.89

Case 4: :Via-last with preplaced substrate contacts

A similar analysis is performed with a via-last TSV and preplaced substrate contacts. The results of this analysis are illustrated in Figures [30 – 35]. The corresponding fitting coefficients are provided in Table 4.

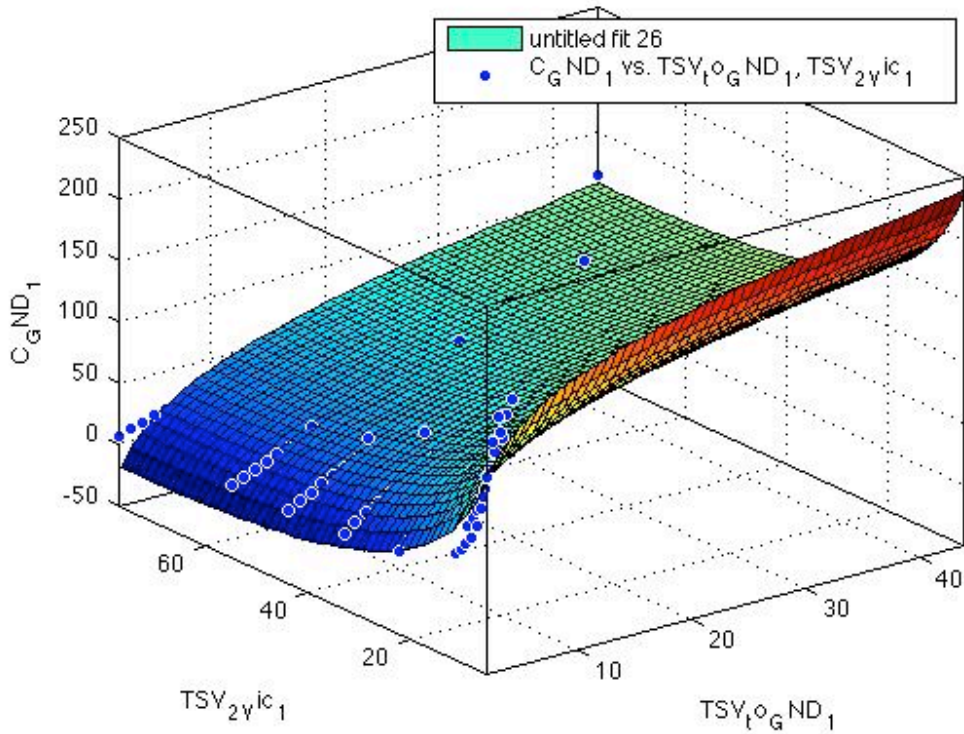


Figure 30-Case 4, C_{GND} vs. $d1$ and $d2$.

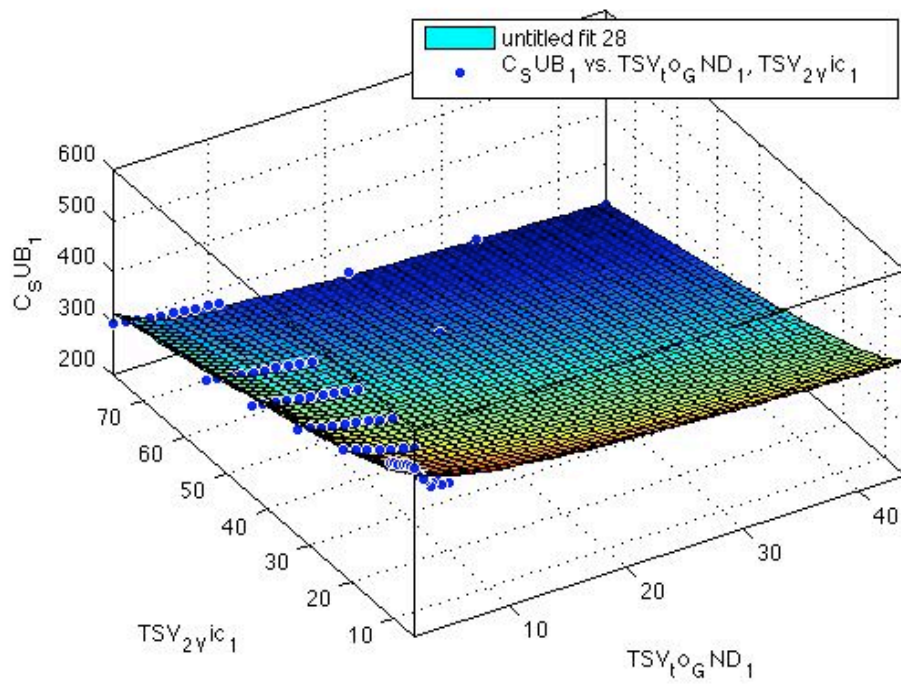


Figure 31-Case 4, C_{SUB} vs. d_1 and d_2 .

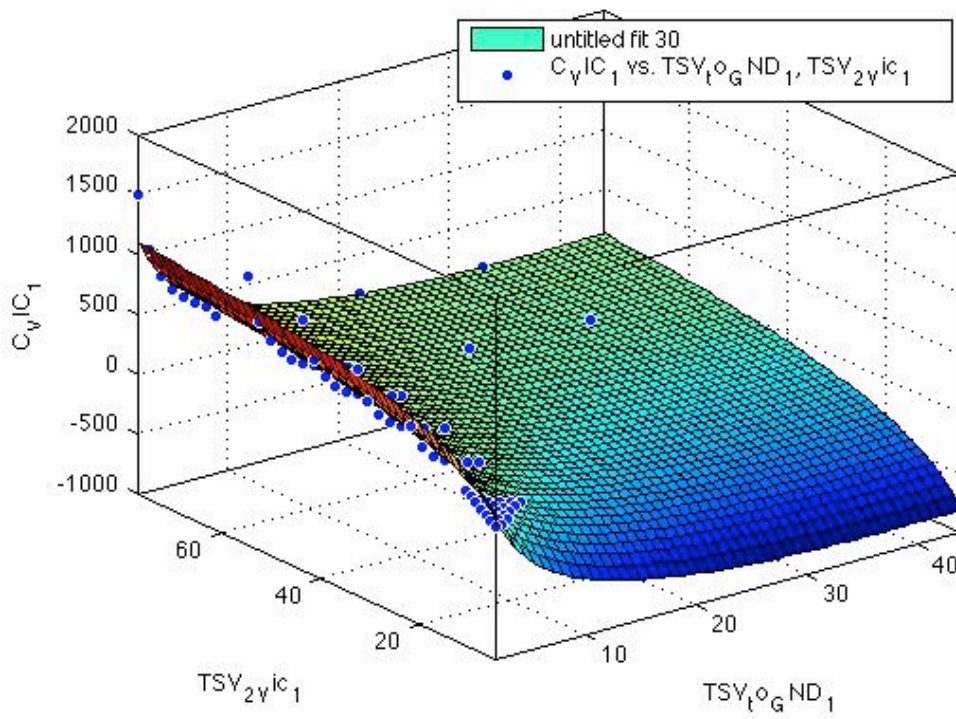


Figure 32-Case 4, C_{VIC} vs. d_1 and d_2 .

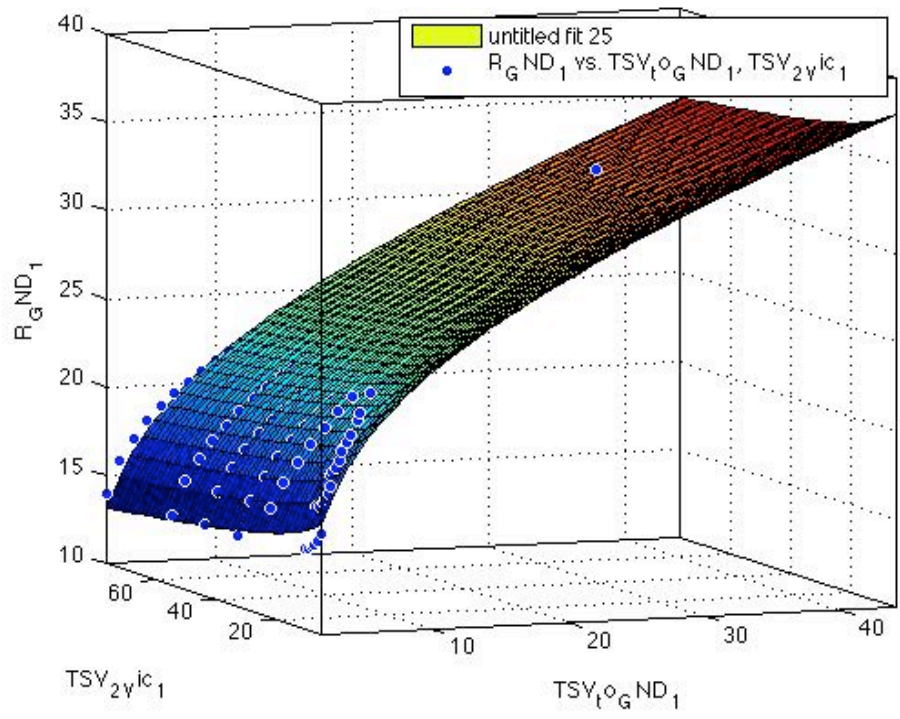


Figure 33-Case 4, $1000/R_{GND}$ vs. d1 and d2.

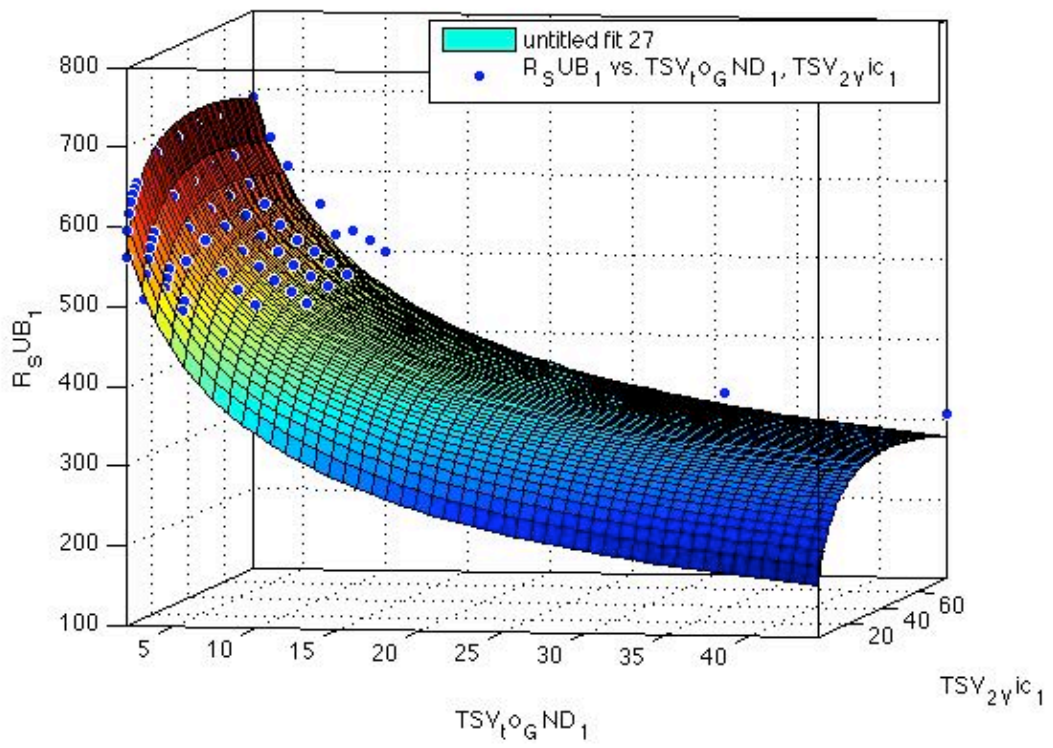


Figure 34-Case 4, $1000/R_{SUB}$ vs. d1 and d2.

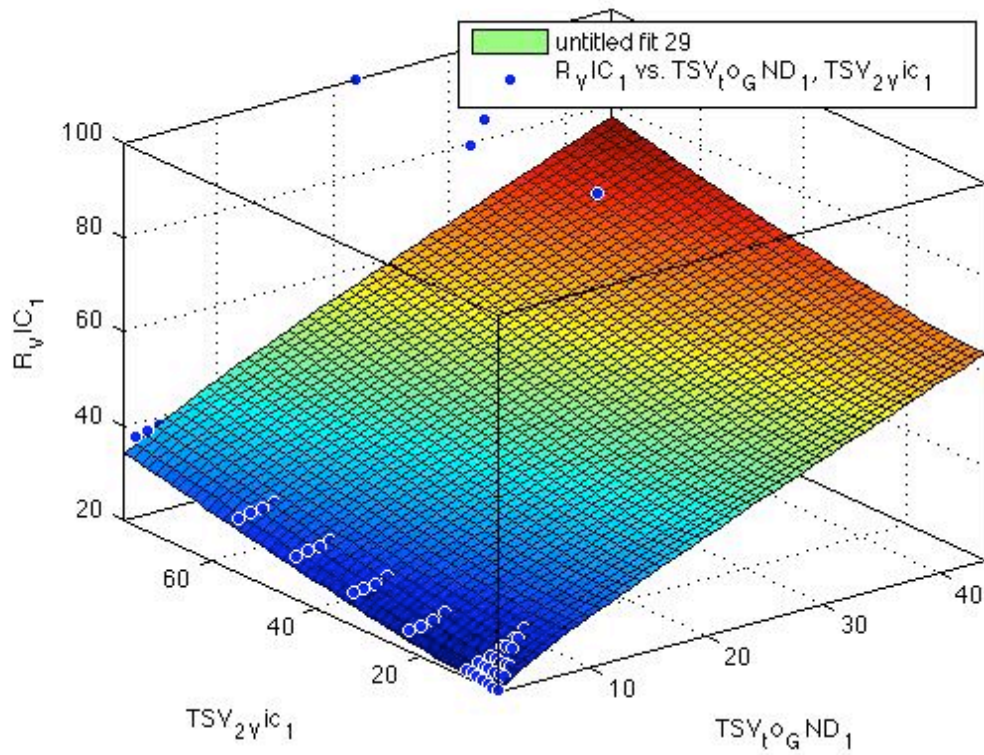


Figure 35-Case 4, R_{VIC} vs. $d1$ and $d2$.

Table 4 - Fitting coefficients Case 4.

	$1000/R_{GND}$ (K Ω)	C_{GND} (af)	R_{SUB} (K Ω)	C_{SUB} (af)	R_{VIC} (K Ω)	C_{VIC} (af)
	$1000/F(d1,d2)$	$F(d1,d2)$	$1000/F(d1,d2)$	$F(d1,d2)$	$F(d1,d2)$	$1000/F(d1,d2)$
A	14.74	67.4	309.8	276.5	3.1	276.5
B	0.333	0.16	0.0789	0.118	0	0
C	0	0.532	-0.971	-0.6835	0	0.87
D	-0.86	-26.48	61.2	-13.4	-6.899	-48.99
E	4.7	8.9	-7.56	-24.3	4.36	20.34

Chapter 5 – Analysis Results and Discussion

Equivalent models are obtained for the four cases as described in the previous chapter. These models are helpful to analyze noise coupling and determine the advantages and limitations of different types of TSVs and ground contact placements. These results provide valuable guidelines to produce reliable 3-D ICs with enhanced signal integrity.

The noise coupling characteristics of via-first and via-last TSVs are compared in Figure 36 when there is only a single ground connection between the TSV and the victim. As shown in this figure, via-last TSVs inject greater noise as compared to via-first TSVs. Similarly, with preplaced substrate contacts in the circuit, the magnitude of the noise transfer function is higher for via-last, as illustrated in Figure 37. This result is due to the higher TSV diameter and depth. A higher diameter and depth significantly increases the TSV capacitance. Furthermore, a greater depth reduces the substrate resistance thereby increasing the noise that couples to the victim.

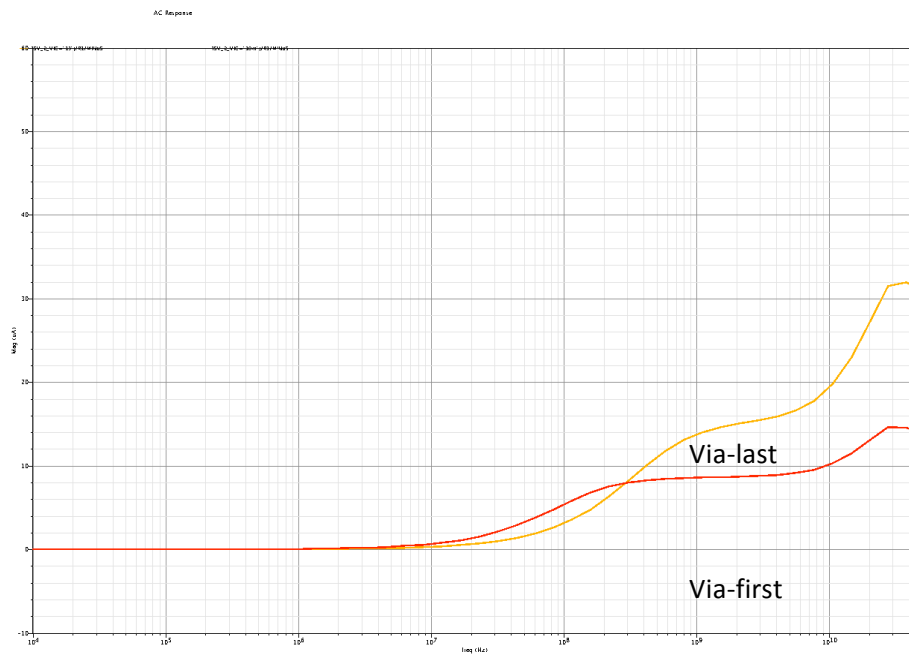


Figure 36 - Noise transfer function, custom single ground.

Another important factor in determining noise behavior is the placement of ground contacts on the substrate. The dependence of noise coupling on the distance between TSV and ground contact is illustrated in Figure 37 in time domain for both via first and via last TSVs, where a time domain analysis is performed. Depending on noise constraints, the peak and RMS noise can be important design objectives. Using the transfer function, the peak noise can be obtained by multiplying the FFT of the input signal with the transfer function and transforming the result back to the time domain. The results obtained from this procedure are the same as transient analysis results.

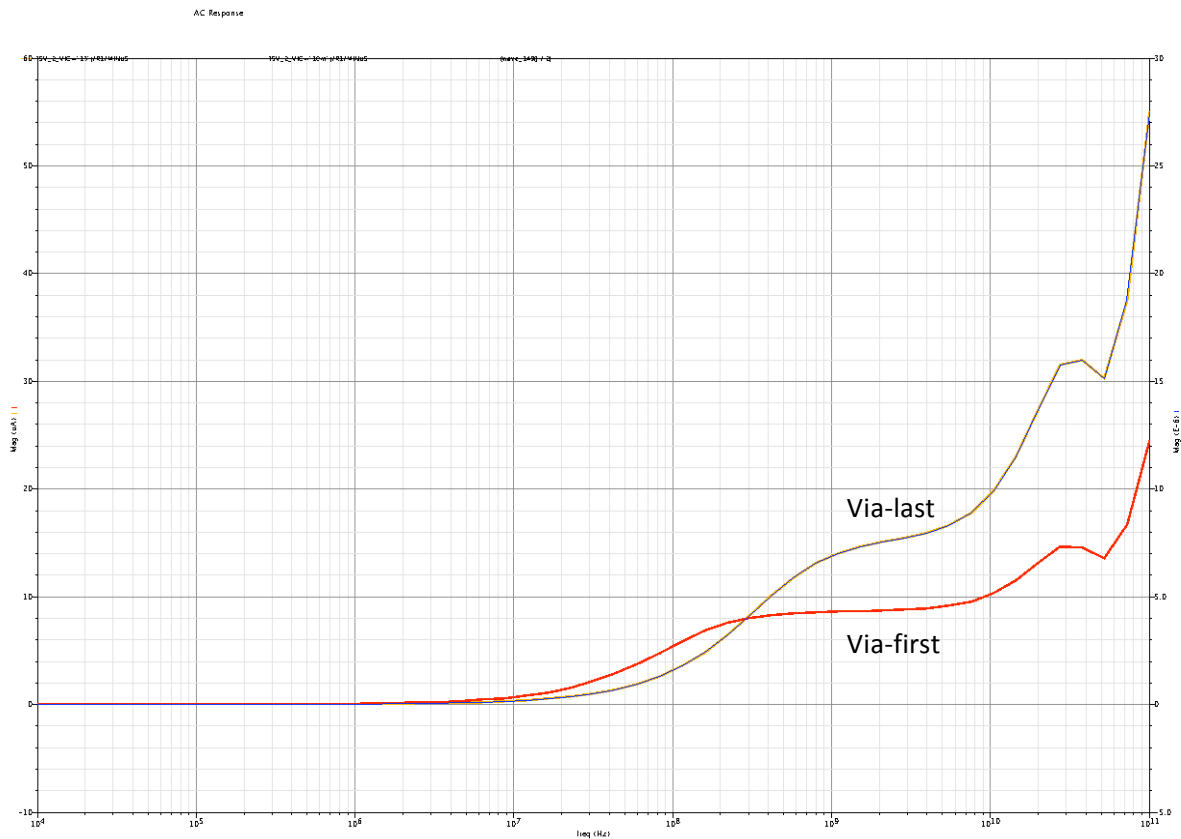


Figure 37 - Noise transfer function, pre-placed ground node.

As illustrated in Figure 38, the noise that couples to the victim initially increases with increasing distance between TSV and ground contact. After a certain point however, the increase in the noise is marginal. Another important conclusion from this figure is that the dependence of noise on distance is stronger for the via-last TSVs. Thus, in via-last TSVs, placing a ground contact sufficiently close to the TSV is important to reduce noise.

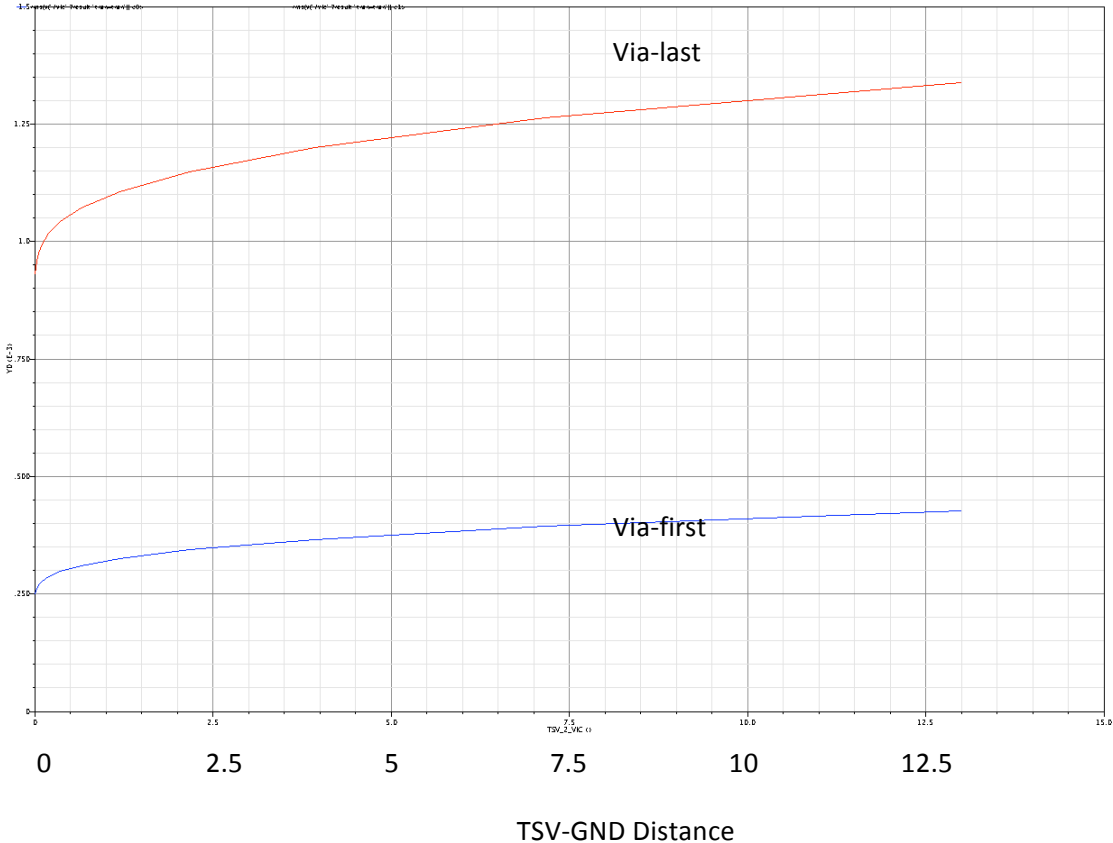


Figure 38 - RMS noise comparison vs. TSV-GND distance. Via-last, Via-first.

Chapter 6 – Conclusions

Among the emerging IC technologies, 3-D integration is widely recognized as a potential candidate to continue technology scaling. This technology utilizes TSVs to transmit data, power, and clock signals to different planes. An adverse effect of the TSVs is noise injection into the substrate. This effect is modeled in this thesis and related design guidelines are provided.

To model the substrate, a complicated distributed network of resistors and capacitors is used as a reference. To model TSV related noise coupling, four different cases are investigated (via-first TSV with a single custom ground connection, via-last TSV with a single custom ground connection, via-first TSV with a distributed ground pattern, and via-last TSV with a distributed ground pattern). Compact equivalent models based on a *pi*-circuit are developed for each case.

The developed noise transfer functions are utilized to investigate the noise characteristics of via-first and via-last TSVs and different ground contact configurations. The proposed models can also be used to determine a safe distance around an aggressor TSV. This safe distance depends on the tolerable noise which is determined by the type and functionality of the circuit. This thesis provides design guidelines to avoid TSV related noise coupling and enhance reliability in 3-D ICs.

Chapter 7 – Future Work

This work can be expanded in several ways. Reliability is a primary concern in nanoscale technologies where the effect of environmental variations such as noise is significant. In dense 3-D circuits, TSV related noise coupling can cause detrimental issues. Using the method described in this thesis, TSV related noise coupling can be efficiently analyzed and the effect of noise can be investigated in specialized circuits such as core-memory stacks and 3-D integrated implantable biomedical circuits.

Another topic that can be further explored is the efficiency of various noise reduction methodologies. For example, the effect of guard rings in suppressing TSV related noise can be modeled for different ring dimensions and topologies. Furthermore, utilizing power and ground TSVs to shield noise can be explored to further minimize noise coupling.

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